

# Digital wave flume using multi-fidelity approaches

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#### **Research Motivation**



Fg.1. Tsunami phenomenon<sup>1</sup>



Fg.2. Hurricane<sup>2</sup>



Fg.3. Floating wind turbine <sup>3</sup>



Fg.4. Ocean wave energy harvest<sup>4</sup>

<sup>1</sup>Crossing <u>swells</u>, consisting of near-cnoidal wave trains. Photo taken from Phares des Baleines (Whale Lighthouse) at the western point of <u>Île de Ré</u> (Isle of Rhé), France, in the <u>Atlantic Ocean</u>.

<sup>2</sup><u>Hurricane Paulette</u>, in <u>2020</u>, is an example of a <u>sheared</u> tropical cyclone, with deep <u>convection</u> slightly removed from the center of the system <sup>3</sup>Wang, C.M., Utsunomiya, T., Wee, S.C. and Choo, Y.S., 2010. Research on floating wind turbines: a literature survey. *The IES Journal Part A: Civil & Structural Engineering*, *3*(4), pp.267-277.

<sup>4</sup> Huang, B., Wang, P., Wang, L., Yang, S. and Wu, D., 2020. Recent advances in ocean wave energy harvesting by triboelectric nanogenerator: An overview. *Nanotechnology Reviews*, *9*(1), pp.716-735.



# Smoothed Particle Hydrodynamics (SPH)<sup>1</sup>



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#### Mesh-based Method

#### **Meshless Method**

- Computational points: Nodes ----- > Particles
- Each particle is associated with **field variables** such as mass, momentum, velocity, position, energy, etc.
- Particles are described through Lagrangian derivatives Rate of change along with the trajectory

<sup>&</sup>lt;sup>1</sup>Gingold, R. A., & Monaghan, J. J. (1977). Smoothed particle hydrodynamics: Theory and application to non-spherical stars. *Monthly Notices of the Royal Astronomical Society*, *181*(3), 375–389

#### **Smoothed Particle Hydrodynamics**



 Each particle has an associated weight determined by a kernel function, which describes the contribution of the neighboring particles to the physical quantities (such as pressure or velocity)



Fig. The concept of Smoothed Particle Hydrodynamics<sup>1</sup>

<sup>1</sup>Dai, Z., Wang, F., Huang, Y., Song, K., & Iio, A. (2016). SPH-based numerical modeling for the post-failure behavior of the landslides triggered by the 2016 Kumamoto earthquake. *Geoenvironmental Disasters*, *3*(1)

#### **Experimental Setup**



Fig. Left: resistance wave gauges and acoustic velocimeters positioned in hydraulic wave flume. Right: instrumented specimen and front side pressure gauges, wave gauge, and acoustic doppler velocimeters. Bottom: Profile views of experimental flume<sup>1</sup>

<sup>1</sup>Tomiczek, T., Prasetyo, A., Mori, N., Yasuda, T., & Kennedy, A. (2016). Physical modelling of tsunami onshore propagation, peak pressures, and shielding effects in an urban building array. *Coastal Engineering*, *117*, 97–112.

- Hybrid Tsunami Open Flume in Ujigawa (HyTOFU) Laboratory, Kyoto University
- 45 m long, 4 m wide, and 2 m deep wave flume, slope 1:10
- A single specimen (building) instrumented with pressure gauges was placed on flat platform
- Solitary waves was generated using wave piston
- Free surface elevation was measured in 10 different locations using resistancetype Wave Gauges

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Fig. 5. HyTOFU DualSPHysics setup

#### Dynamic boundary conditions<sup>1</sup>

- domain → particles
- Grey particles solid particles (walls, building)
- Red particles moving particles (piston wavemaker)
- Blue particles fluid particles (water)

# **Numerical Setup**

Wave parameters

Still water depth - 0.7m Wave type - Solitary wave Wave height - 0.4m



Wave gauge

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 WG6 (x=22.69)
 0.79
 0.40

 WG5 (x=21.50)
 WG4 (x=20.50)
 0.79
 0.40

 WG3 (x=17.50)
 WG2 (x=14.50)
 0
 0

 WG1 (x=9.15)
 0
 0
 0

 WG8 (x=22.99)
 0
 0
 0

 WG1 (x=24.09)
 WG1 (x=24.89)
 0
 0



Fig. HyTOFU set up with the location of the wave gauges

<sup>1</sup>Crespo, A. J. C., Domínguez, J. M., Rogers, B. D., Gómez-Gesteira, M., Longshaw, S., Canelas, R., Vacondio, R., Barreiro, A., & García-Feal, O. (2015). DualSPHysics: Open-source parallel CFD solver based on Smoothed Particle Hydrodynamics (SPH). *Computer Physics Communications*, *187* 

## **Convergence study**



Fig. Convergence study associated with wave gauges 1, 2 and 3

•	Initial interparticle distance (dp) Wave height (W) = 0.4 m	dp	H/dp	Error in peak height	Error in wave arrival time	Compute time
		0.1	4	8.87 %	-2.20 %	78.51s
•	dp = 0.0125m showed superior	0.025	16	1.96 %	-3.14 %	97854s
	agreement with experimental data	0.0125	32	1.86 %	1.57 %	110534s

# **Smoothened Particle Hydrodynamics: Results**



Free surface elevation agreement is observed in initial flat and sloping sections (WG1, WG2, WG3) and test section (WG4, WG5)

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- Unable to validate accuracy of free surface elevation representation in front (WG6) and back (WG9) of the specimen due to limitations in data recording
- Overall. wave arrival time
   and wave height show
   effective validation of the
   numerical model

1/25/2024

Fig. 7. Comparison of free surface elevation data

# Wave loading evaluation



![](_page_8_Picture_2.jpeg)

- Comparison of different methods for evaluation of structural response (a)
- Forces evaluated using different wave heights
  - SPH model (b)
  - ASCE (c)
  - Analytical (d)

Why maximum drag force does not consistently increase as initial wave height increase?

Fig. 8. Evaluation of wave loading with different initial wave heights

# **Build 25 wave gauges**

![](_page_9_Picture_1.jpeg)

To check if there is breaking point and dissipation happens in different initial wave height case

![](_page_9_Figure_3.jpeg)

- Same: Initial wave height = 0.4m, 0.9m
- Big dump: Initial wave height = 0.5m, 0.6m
- Little dump: Initial wave height = 0.7m, 0.8m

# **Uncertainty Quantification**

![](_page_10_Picture_1.jpeg)

![](_page_10_Figure_3.jpeg)

# **Uncertainty Quantification**

![](_page_11_Picture_1.jpeg)

- Probabilistic structural dynamic analyses are performed to identify the realistic range of building responses
- Provides more reliable estimates for practical engineering applications
- Uncertainties in structural responses typically arise from two primary sources
- 1. Parameters associated with coastal wave
- 2. Parameters associated with building (structures)

**Forward UQ (Structures) :** Quantifies the uncertainty in output parameters by propagating the uncertainties present in selected input parameters

![](_page_11_Figure_8.jpeg)

Structural input uncertainty

Structural response probability

# **Forward UQ: Inputs**

**Random Variables** 

![](_page_12_Picture_2.jpeg)

![](_page_12_Figure_3.jpeg)

![](_page_13_Figure_0.jpeg)

![](_page_13_Figure_1.jpeg)

- Notable concentration around middle of acceleration range
- Mean =  $0.0010 \text{ m/s}^2$ Standard deviation = 0.0001 m/s<sup>2</sup>

![](_page_13_Figure_4.jpeg)

MANCHESTER The University of Manchester Yield strength versus peak floor acceleration and stiffens versus peak

floor acceleration plots displayed a random distribution with **no** discernible correlation

Floor weight exhibited a strong negative correlation with peak floor acceleration

![](_page_14_Picture_1.jpeg)

![](_page_14_Figure_2.jpeg)

![](_page_15_Picture_1.jpeg)

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#### Reduce domain size

![](_page_15_Figure_4.jpeg)

![](_page_16_Picture_1.jpeg)

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Reduce domain size & Simulate more cases

![](_page_16_Figure_4.jpeg)

![](_page_17_Picture_1.jpeg)

![](_page_17_Figure_3.jpeg)

# Graph Sample and Aggregate (GraphSAGE)

![](_page_18_Picture_1.jpeg)

![](_page_18_Figure_2.jpeg)

# **GraphSAGE in Wave Propagation Prediction**

![](_page_19_Picture_1.jpeg)

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Advantage for using GraphSAGE:

- Considering the relationships between nodes
- Incorporating node features
- Learning node embeddings
- Predictive capability

	Train_x	Train_y	1.0 -	WG5	-*- WH 0.8 (SPH)
Training set (Initial wave height 0.4m)	Wave Gauge 4	Wave Gauge 5	0.8 -		
Validation set (Initial wave height 0.5m)	Wave Gauge 4	Wave Gauge 5	0.6 - E g. 0.4 -		
Testing set (Initial wave height 0.8m and 0.9m)	Wave Gauge 4	Wave Gauge 5	0.2 -		
				t (ms)	

#### **GraphSAGE in Wave Propagation Prediction**

![](_page_20_Picture_1.jpeg)

![](_page_20_Figure_3.jpeg)

![](_page_21_Picture_0.jpeg)

# **GraphSAGE at Wave gauge 5**

![](_page_21_Figure_2.jpeg)

- The arrival time values are not important
   Structural response is not depending on arrival time
- Wave form is only important information! as we use this as boundary conditions to CFD

#### Conclusions

- Full fidelity CFD simulations are computationally expensive
- Proposed a promising methodology by augment surrogate model with CFD to reduced computational cost without accuracy lost
- Wave form has been successfully captured using GraphSAGE
- Coupling UQs with CFD simulations gives more realistic range of building responses

# **Future Work**

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![](_page_23_Figure_3.jpeg)

![](_page_24_Picture_0.jpeg)

#### **Future Work**

![](_page_24_Figure_2.jpeg)

## Appendix 1

![](_page_25_Figure_1.jpeg)

- (a) WG1
  (b) WG2
  (c) WG3
  (d) WG4
  (e)WG5
  (f) WG7
- (g) WG8
- (h) WG9
- (i) WG10

Fig. Free surface elevation for different wave heights for wave gauges